CHAPTER 90

USE OF A COMPUTATIONAL MODEL FOR TWO-DIMENSIONAL TIDAL FLOW

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INTRODUCTION

The numerical solution of tidal hydraulic problems has been greatly fa-
cilitated in the last decade by the development of high-speed large-memory
computers. Problems which only could be studied by use of hydraulic models
can now readily be studied with mathematical models if the computational tech-
niques for solutions are developed.

Unfortunately the difficulties in formulating usable methods for these
complicated problems in fluid dynamics are formidable, particularly if the
problems are multidimensional in space. As a result the numerical solution
approach to these hydraulic problems has generally been limited and has not
kept pace with the increased capabilities of the presently available compu-
ters.

In this paper a new approach is given to the solution of two-dimensional
tidal flow in shallow water.

THE DIFFERENTIAL EQUATIONS REPRESENTING TIDAL FLOW

The basis of the computational model for tidal flow is the long-period
water-wave equations (ref. 1):

$$\frac{\partial U}{\partial t} + U \frac{\partial U}{\partial x} + V \frac{\partial U}{\partial y} - fV + g \frac{\partial \zeta}{\partial x} + g \frac{U(U^2 + V^2)^{\frac{1}{2}}}{C^2(h + \zeta)} = 0 \tag{1}$$

$$\frac{\partial V}{\partial t} + U \frac{\partial V}{\partial x} + V \frac{\partial V}{\partial y} + fU + g \frac{\partial \zeta}{\partial y} + g \frac{V(U^2 + V^2)^{\frac{1}{2}}}{C^2(h + \zeta)} = 0 \tag{2}$$

$$\frac{\partial \zeta}{\partial t} + \frac{\partial [(h + \zeta)U]}{\partial x} + \frac{\partial [(h + \zeta)V]}{\partial y} = 0 \tag{3}$$

Symbols are defined as follows:

U, V : vertically integrated velocity components in the x and y
      direction respectively
ζ : elevation of the free surface over the undisturbed level
h : depth
g : acceleration due to gravity
f : Coriolis parameter
C : Chezy coefficient

THE SYSTEM OF THE FINITE-DIFFERENCE EQUATIONS IN TWO DIMENSIONS

The following notation is used in the approximation of the differential equations:

$$u_{j,k}^{(n)} \equiv U(j\Delta x, \; k\Delta y, \; n\Delta t); \qquad \Delta x = \Delta y = \Delta s \tag{4}$$

where

$(x,y) = (j\Delta x, \; k\Delta y)$ and is a spatial grid point

$j,k = 0, \; \pm \tfrac{1}{2}, \; \pm 1, \; \pm 3/2, \; \ldots$

$n = 0, \; \tfrac{1}{2}, \; 1, \; 3/2, \; 2$

Furthermore, the following notation of averages and differences shown here for ζ, is introduced:

$$\overline{\zeta}_{j,k}^{x} = \tfrac{1}{2} \, (\zeta_{j+\frac{1}{2},k} + \zeta_{j-\frac{1}{2},k}) \tag{5}$$

$$\zeta_{x} = (\zeta_{j+\frac{1}{2},k} - \zeta_{j-\frac{1}{2},k}) \tag{6}$$

$$\overline{\zeta}_{j,k}^{y} = \tfrac{1}{2} \, (\zeta_{j,k+\frac{1}{2}} + \zeta_{j,k-\frac{1}{2}}) \tag{7}$$

$$\zeta_{y} = (\zeta_{j,k+\frac{1}{2}} - \zeta_{j,k-\frac{1}{2}}) \tag{8}$$

$$\overline{\zeta}_{j,k} = \tfrac{1}{4} \, (\zeta_{j-\frac{1}{2},k-\frac{1}{2}} + \zeta_{j-\frac{1}{2},k+\frac{1}{2}} + \zeta_{j+\frac{1}{2}, \; k-\frac{1}{2}} + \zeta_{j+\frac{1}{2},k+\frac{1}{2}}) \tag{9}$$

A space-staggered scheme is used where velocities, water levels, and depth are described at different grid points (see Fig. 1). This scheme has the advantage that for the variable operated upon in time, there is a centrally located spatial derivative.

In time, a multistep operation is used in such a manner that the terms containing space derivatives and the Coriolis force are generally taken alternating forward and backward.

The individual operations each have two time levels. The first operation is taken from time n to time $n+\tfrac{1}{2}$, and the second operation is taken from time $n+\tfrac{1}{2}$ to time n+1. Values of the fields of ζ, u, and v at time $n+\tfrac{1}{2}$ are obtained from the fields of ζ, u, and v at time n by an operation which is implicit in ζ and u and explicit in v. Then the fields of ζ, u, and v at time n+1 are computed from the fields of ζ, u, and v at time $n+\tfrac{1}{2}$ by an operation which is implicit in ζ and v and explicit in u. The two sets of difference equations of this multioperation method are now written with the equation of continuity aa the second equation of each set (Eqs. 11, 14), using an integer value for j and k and maintaining the velocity gradients in the convective-inertia terms in differential form within angle brackets < >. The effects of bottom roughness are indicated by a function R. Thus, for the first operation the equations are:
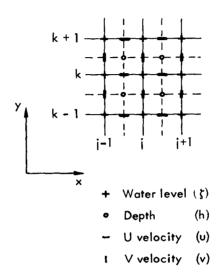
+ Water level (ζ)

o Depth (h)

— U velocity (u)

ı V velocity (v)

Fig. 1—Space-staggered scheme

$$u^{(n+\frac{1}{2})} = u(n) + \tfrac{1}{2}\,\Delta t\,f\bar{\bar{v}}^{(n)} - \tfrac{1}{2}\,\Delta t\,u^{(n+\frac{1}{2})}\,\big\langle\tfrac{\partial u}{\partial x}\big\rangle^{(n)} - \tfrac{1}{2}\,\Delta t\,\bar{\bar{v}}^{(n)}\,\big\langle\tfrac{\partial u}{\partial y}\big\rangle^{(n)}$$

$$- \tfrac{1}{2}\,\tfrac{\Delta t}{\Delta s}\,g\zeta_x^{(n+\frac{1}{2})} - R(x)^{(n)} \qquad\qquad \text{at } j + \tfrac{1}{2},\ k \qquad\qquad (10)$$

$$\zeta^{(n+\frac{1}{2})} = \zeta^{(n)} - \tfrac{1}{2}\,\tfrac{\Delta t}{\Delta s}\,[(\bar{h}^y + \zeta^x)^* u]_x^{(n+\frac{1}{2})} - \tfrac{1}{2}\,\tfrac{\Delta t}{\Delta s}\,[(\bar{h}^x + \zeta^y)v]_y^{(n)}$$

$$\text{at } j,\ k \qquad\qquad (11)$$

$$v^{(n+\frac{1}{2})} = v^{(n)} - \tfrac{1}{2}\,\Delta t\,f\bar{\bar{u}}^{(n+\frac{1}{2})} - \tfrac{1}{2}\,\Delta t\,\bar{\bar{u}}^{(n+\frac{1}{2})}\,\big\langle\tfrac{\partial v}{\partial x}\big\rangle^{(n)}$$

$$-\tfrac{1}{2}\,\Delta t v^{(n+\frac{1}{2})}\,\big\langle\tfrac{\partial v}{\partial x}\big\rangle^{(n)} - \tfrac{1}{2}\,\tfrac{\Delta t}{\Delta s}\,g\zeta_y^{(n)} - R(y)^{(n+\frac{1}{2})}{}_{j,k+\frac{1}{2}} \qquad\qquad (12)$$

For the second operation, the equations are:

$$u^{(n+1)} = u^{(n+\frac{1}{2})} + \tfrac{1}{2}\,\Delta t\,f\bar{\bar{v}}^{(n+1)} - \tfrac{1}{2}\,\Delta t\,u^{(n+1)}\,\big\langle\tfrac{\partial u}{\partial x}\big\rangle^{(n+\frac{1}{2})}$$

$$- \tfrac{1}{2}\,\Delta t\,\bar{\bar{v}}^{(n+1)}\big\langle\tfrac{\partial u}{\partial y}\big\rangle^{(n+\frac{1}{2})} - \tfrac{1}{2}\,\tfrac{\Delta t}{\Delta s}\,g\zeta_x^{(n+\frac{1}{2})} - R(x)^{(n+1)}$$

$$\text{at } j + \tfrac{1}{2},\ k \qquad\qquad (13)$$

$$\zeta^{(n+1)} = \zeta^{(n+\frac{1}{2})} - \tfrac{1}{2}\,\tfrac{\Delta t}{\Delta s}\,[(\bar{h}^y + \zeta^x)u]_x^{(n+\frac{1}{2})} - \tfrac{1}{2}\,\tfrac{\Delta t}{\Delta s}\,[(\bar{h}^x + \zeta^y)^* v]_y^{(n+1)}$$

$$\text{at } j,k \qquad\qquad (14)$$

$$v^{(n+1)} = v^{(n+\frac{1}{2})} - \tfrac{1}{2}\,\Delta t\,f\bar{\bar{u}}^{(n+\frac{1}{2})} - \tfrac{1}{2}\,\Delta t\,\bar{\bar{u}}^{(n+\frac{1}{2})}\big\langle\tfrac{\partial v}{\partial x}\big\rangle^{(n+\frac{1}{2})}$$

$$- \tfrac{1}{2}\,\Delta t\,v^{(n+1)}\big\langle\tfrac{\partial v}{\partial y}\big\rangle^{(n+\frac{1}{2})} - \tfrac{1}{2}\,\tfrac{\Delta t}{\Delta s}\,g\zeta_y^{(n+1)} - R(y)^{(n+\frac{1}{2})}$$

$$\text{at } j,\ k + \tfrac{1}{2} \qquad\qquad (15)$$

where

$$\big\langle\tfrac{\partial u}{\partial x}\big\rangle_{j+\frac{1}{2},k} = \tfrac{1}{2\Delta s}\,(u_{j+\frac{3}{2},k} - u_{j-\frac{1}{2},k}) \qquad\qquad (16)$$

$$\big\langle\tfrac{\partial u}{\partial y}\big\rangle_{j+\frac{1}{2},k} = \tfrac{1}{2\Delta s}\,(u_{j+\frac{1}{2},k+1} - u_{j+\frac{1}{2},k-1}) \qquad\qquad (17)$$

$$\big\langle\tfrac{\partial v}{\partial x}\big\rangle_{j,k+\frac{1}{2}} = \tfrac{1}{2\Delta s}\,(v_{j+1,k+\frac{1}{2}} - v_{j-1,k+\frac{1}{2}}) \qquad\qquad (18)$$

$$\big\langle\tfrac{\partial v}{\partial y}\big\rangle_{j,k+\frac{1}{2}} = \tfrac{1}{2\Delta s}\,(v_{j,k+\frac{3}{2}} - v_{j,k-\frac{1}{2}}) \qquad\qquad (19)$$

$$R(x)^{(n)} = \frac{1}{2} \Delta t \ gu^{(n)} \frac{\sqrt{(u^{(n)})^2 + (\bar{\bar{v}}^{(n)})^2}}{(\bar{h}^y + \zeta^{x(n)})(C^x)^2} \qquad \text{at } j + \frac{1}{2}, \ k \qquad (20)$$

$$R(y)^{(n+\frac{1}{2})} = \frac{1}{2} \Delta t \ gv^{(n+\frac{1}{2})} \frac{\sqrt{(\bar{\bar{u}}^{(n+\frac{1}{2})})^2 + (v^{(n)})^2}}{(\bar{h}^x + \zeta^{y(n+\frac{1}{2})})(C^y)^2} \qquad \text{at } j, \ k + \frac{1}{2} \qquad (21)$$

$$R(x)^{(n+1)} = \frac{1}{2} \Delta t \ gu^{(n+1)} \frac{\sqrt{(u^{(n+\frac{1}{2})})^2 + (\bar{\bar{v}}^{(n+1)})^2}}{(\bar{h}^y + \zeta^{x(n+1)})(C^x)^2} \qquad \text{at } j + \frac{1}{2}, \ k \qquad (22)$$

$$R(y)^{(n+\frac{1}{2})} = \frac{1}{2} \Delta t \ gv^{(n+\frac{1}{2})} \frac{\sqrt{(\bar{\bar{u}}^{(n+\frac{1}{2})})^2 + (v^{(n+\frac{1}{2})})^2}}{(\bar{h}^x + \zeta^{y(n+\frac{1}{2})})(C^y)^2} \qquad \text{at } j, \ k + \frac{1}{2} \qquad (23)$$

A special, additional technique will be employed for the computation of the nonlinear terms marked with an asterisk.

Solutions of the Equations (10-15) are found by direct computation or by solving systems of equations which relate water levels and velocities on lines.

In each of Eqs. (10) and (11) there are three values at the time level (n + ½), which are all situated at the line k and have to be computed. Writing the continuity equation first and omitting the subscript k, we can write Eqs. (10) and (11) in the following form:

$$-\frac{1}{2} \frac{\Delta t}{\Delta s} [(\bar{h}^y + \zeta^x)^* u]_{j-\frac{1}{2}}^{(n+\frac{1}{2})} = \zeta_j^{(n+\frac{1}{2})} + \frac{1}{2} \frac{\Delta t}{\Delta s} [(\bar{h}^y + \zeta^x)^* u]_{j+\frac{1}{2}}^{(n+\frac{1}{2})} = A_j^{(n)} \qquad (24)$$

$$-\frac{1}{2} \frac{\Delta t}{\Delta s} g\zeta_j^{(n+\frac{1}{2})} + (1 + \frac{1}{4} \frac{\Delta t}{\Delta s} \left(u_{j+\frac{1}{2}}^{(n)} - u_{j-\frac{1}{2}}^{(n)} \right) u_{j+\frac{1}{2}}^{(n+\frac{1}{2})} + \frac{1}{2} \frac{\Delta t}{\Delta s} g\zeta_{j+1}^{(n+\frac{1}{2})} = B_{j+\frac{1}{2}}^{(n)} \qquad (25)$$

where

$$A_j^{(n)} = \zeta^{(n)} - \frac{1}{2} \frac{\Delta t}{\Delta s} [(\bar{h}^x + \zeta^y)v]_y^n \qquad \text{at } j, \ k \qquad (26)$$

$$B_{j+\frac{1}{2}}^{(n)} = u^{(n)} + \frac{1}{2} [\Delta t \ f - \frac{\Delta t}{2\Delta s} (u_{j+\frac{1}{2},k+1}^{(n)} - u_{j+\frac{1}{2},k-1}^{(n)})]\bar{\bar{v}}^{(n)}$$

$$- \frac{1}{2} \Delta t \ gu^{(n)} \frac{\sqrt{(u^{(n)})^2 + (\bar{\bar{v}}^{(n)})^2}}{(\bar{h}^y + \zeta^{x(n)})(C^x)^2} \qquad \text{at } j + \frac{1}{2}, \ k \qquad (27)$$

Thus, one equation with three unknowns exists for each velocity field point ($u_{j+\frac{1}{2}}$) and each water level field point (ζ) on a line k. If a row of N water level points is on the line and velocities are given at the boundaries outside of the water levels concerned, N water levels and N - 1 velocities at time (n + ½) must be solved from 2N - 1 equations.

We now introduce

$$r_{j-\frac{1}{2}} = \frac{1}{2}\frac{\Delta t}{\Delta s}\ (\bar{h}^y + \zeta^x)^*_{j-\frac{1}{2}};\ r_{j+\frac{1}{2}} = \frac{1}{2}\frac{\Delta t}{\Delta s}\ (\bar{h}^y + \zeta^x)^*_{j+\frac{1}{2}},\ \ldots \tag{28}$$

$$r_j = \frac{1}{2}\frac{\Delta t}{\Delta s}\ g;\ r_{j+1} = \frac{1}{2}\frac{\Delta t}{\Delta s}\ g;\ \ldots \tag{29}$$

Equations (24) and (25) can be written in matrix form for a line k, assuming that $u_{J-\frac{1}{2}}$ is a given velocity at the lower boundary and $u_{I+\frac{1}{2}}^{(n+\frac{1}{2})}$ is a given velocity at the upper boundary:

$$
\begin{bmatrix}
1 & r_{J+\frac{1}{2}} & 0 & 0 & . & 0 \\
-r_J & a_{J+\frac{1}{2}} & r_{J+1} & 0 & . & 0 \\
0 & -r_{J+\frac{1}{2}} & 1 & r_{J+\frac{3}{2}} & . & 0 \\
. & . & . & . & . & . \\
. & . & . & . & . & . \\
. & . & . & . & . & . \\
0 & 0 & 0 & \ldots & -r_{I-\frac{1}{2}} & 1
\end{bmatrix}
\begin{bmatrix}
\zeta_J \\
u_{J+\frac{1}{2}} \\
\zeta_{J+1} \\
. \\
. \\
. \\
\zeta_I
\end{bmatrix}^{(n+\frac{1}{2})}
=
\begin{bmatrix}
A_J \\
B_{J+\frac{1}{2}} \\
A_{J+1} \\
. \\
. \\
. \\
A_I
\end{bmatrix}^{(n)}
+
\begin{bmatrix}
r_{J-\frac{1}{2}}\ u_{J-\frac{1}{2}} \\
0 \\
0 \\
0 \\
. \\
. \\
r_{I+\frac{1}{2}}\ u_{I+\frac{1}{2}}
\end{bmatrix}^{(n+\frac{1}{2})}
\tag{30}
$$

where

$$a_{J+\frac{1}{2}} = 1 + \frac{1}{4}\frac{\Delta t}{\Delta s}\left(u_{J+\frac{3}{2}}^{(n)} - u_{J-\frac{1}{2}}^{(n)}\right) \tag{31}$$

The values of the vector $(\zeta_J,\ u_{J+\frac{1}{2}},\ \zeta_{J+1},\ \ldots,\ \zeta_I)$ at the n + ½ time level can be solved with a limited number of operations by a process of elimination of unknowns. Starting with the first equation, the water level $\zeta_J^{n+\frac{1}{2}}$ is expressed as a function of the unknown velocity $u_{J+\frac{1}{2}}$:

$$\zeta_J^{(n+\frac{1}{2})} = -P_J u_{J+\frac{1}{2}}^{(n+\frac{1}{2})} + Q_J \tag{32}$$

where

$$P_J = r_{J+\frac{1}{2}} \tag{33}$$

$$Q_J = A_J^{(n)} + r_{J-\frac{1}{2}}\ u_{J-\frac{1}{2}}^{(n+\frac{1}{2})} \tag{34}$$

Substitution of Eq. (32) into the second equation of (30) gives

$$-r_J(-P_J u_{J+\frac{1}{2}}^{(n+\frac{1}{2})} + Q_J) + \left(1 + \frac{1}{4}\frac{\Delta t}{\Delta s}(u_{J+\frac{3}{2}}^{(n)} - u_{J-\frac{1}{2}}^{(n)})\right)u_{J+\frac{1}{2}}^{(n+\frac{1}{2})} + r_{J+1}^{(n+\frac{1}{2})}\ \zeta_{J+1}^{(n+\frac{1}{2})} = B_{J+\frac{1}{2}}^{(n)} \tag{35}$$

or expressing $u_{J+\frac{1}{2}}^{(n+\frac{1}{2})}$ as a function of $\zeta_{J+1}^{(n+\frac{1}{2})}$ gives

$$u_{J+\frac{1}{2}}^{(n+\frac{1}{2})} = -R_J \zeta_{J+1}^{(n+\frac{1}{2})} + S_J \tag{36}$$

where

$$R_J = \frac{r_{J+1}}{\left[1 + r_J P_J + \frac{1}{4} \frac{\Delta t}{\Delta s} \left(u_{J+\frac{3}{2}}^{(n)} - u_{J-\frac{1}{2}}^{(n)}\right)\right]} \tag{37}$$

$$S_J = \frac{B_{J+\frac{1}{2}}^{(n)} + r_J Q_J}{\left[1 + r_J P_J + \frac{1}{4} \frac{\Delta t}{\Delta s} \left(u_{J+\frac{3}{2}}^{(n)} - u_{J-\frac{1}{2}}^{(n)}\right)\right]} \tag{38}$$

Again, the water level can be expressed as a function of the next velocity:

$$\zeta_{J+1} = -P_{J+1} u_{J+\frac{3}{2}}^{n+\frac{1}{2}} + Q_{J+1} \tag{39}$$

where

$$P_{J+1} = \frac{r_{J+\frac{3}{2}}}{1 + r_{J+\frac{1}{2}} R_J} \tag{40}$$

$$Q_{J+1} = \frac{A_{J+1}^{(n)} + r_{J+\frac{1}{2}} S_J}{1 + r_{J+\frac{1}{2}} R_J} \tag{41}$$

Generally, the following recursion formulas can be written

$$\zeta_j^{(n+\frac{1}{2})} = -P_j u_{j+\frac{1}{2}}^{(n+\frac{1}{2})} + Q_j \tag{42}$$

$$u_j^{(n+\frac{1}{2})} = -R_{j-1} \zeta_j^{(n+\frac{1}{2})} + S_{j-1} \tag{43}$$

where

$$P_j = r_{j+\frac{1}{2}}/(1 + r_{j-\frac{1}{2}} R_{j-1}) \tag{44}$$

$$Q_j = (A_j^{(n)} + r_{j-\frac{1}{2}} S_{j-1})/(1 + r_{j-\frac{1}{2}} R_{j-1}) \tag{45}$$

$$R_j = r_{j+1}/[1 + r_j P_j + \frac{1}{4} \frac{\Delta t}{\Delta s} (u_{j+\frac{3}{2}}^{(n)} - u_{j-\frac{1}{2}}^{(n)})] \tag{46}$$

$$S_j = (B_{j+\frac{1}{2}}^{(n)} + r_j Q_j)/[1 + r_j P_j + \frac{1}{4} \frac{\Delta t}{\Delta s} (u_{j+\frac{3}{2}}^{(n)} - u_{j-\frac{1}{2}}^{(n)})] \tag{47}$$

The recursion factors P, Q, R, and S can be computed in succession until
the other bound is reached. If $u_{1+\frac{1}{2}}^{(n+\frac{1}{2})}$ is a given velocity, the last two
factors computed are P_I and Q_I. Since Eq. (42) expresses ζ_I as a known
function of the velocity $u_{1+\frac{1}{2}}^{(n+\frac{1}{2})}$, ζ_I can be computed, and all water levels
and velocities can be found in descending order by use of Eqs. (42) and (43).

The nonlinear terms in the continuity equation which are marked with
an asterisk can be computed on their proper time level by an iteration
procedure. The first estimate of $\zeta^{(n+\frac{1}{2})}$ is made by the implicit procedure
of taking the nonlinear term at the time level n. Next, the value $\zeta^{(n+\frac{1}{2})}$
thus computed is used in Eq. (11) for the actual computation. This itera-
tion can be repeated several times. Use of the mathematical model, however,
indicated that no gain in accuracy is obtained.

The velocity in the other direction at the time level n + ½ can be
found explicitly from Eq. (12), since the velocity $u^{(n+\frac{1}{2})}$ in the Coriolis
term is already known. Eq. (12) can then be written:

$$v^{(n+\frac{1}{2})} = \frac{\left\{ v^{(n)} - \frac{1}{2} \left[\Delta t \ f + \frac{1}{2} \frac{\Delta t}{\Delta s} (v_{j+1,k+\frac{1}{2}}^{(n)} - v_{j-1,k+\frac{1}{2}}^{(n)}) \right] \bar{\bar{u}}^{(n+\frac{1}{2})} - \frac{1}{2} \frac{\Delta t}{\Delta s} g \zeta_y^{(n)} \right\}}{\left[1 + \frac{1}{2} \Delta t \ g \ \frac{\sqrt{(\bar{\bar{u}}^{(n+\frac{1}{2})})^2 + (v^{(n)})^2}}{(\bar{h}^x + \zeta^{y(n+\frac{1}{2})})(C^y)^2} + \frac{1}{4} \frac{\Delta t}{\Delta s} (v_{j,k+\frac{3}{2}}^{(n)} - v_{j,k-\frac{1}{2}}^{(n)}) \right]}$$

$$\text{at } j, \ k + \tfrac{1}{2} \quad (48)$$

For the second operation, going from the time level n + ½ to n + 1, Eqs.
(14) and (15) are solved implicitly in the same manner as described for
Eq. (10) and (11). Finally, the velocity in the x-direction can be compu-
ted explicitly from Eq. (13). It can be seen that no more than two suc-
cessive fields have to be stored in the computer memory, as only the lat-
est information available is necessary to compute the next step.

The coefficients for the recursion formulas in the y-direction are

$$P_k = r_{k+\frac{1}{2}}/(1 + r_{k-\frac{1}{2}}R_{k-1}) \tag{49}$$

$$Q_k = (A_k^{(n+\frac{1}{2})} + r_{k-\frac{1}{2}}S_{k-1})/(1 + r_{k-\frac{1}{2}}R_{k-1}) \tag{50}$$

$$R_k = r_{k+1}/[1 + r_kP_k + \frac{1}{4}\frac{\Delta t}{\Delta s}(v_{k+\frac{3}{2}}^{(n+\frac{1}{2})} - v_{k-\frac{1}{2}}^{(n+\frac{1}{2})})] \tag{51}$$

$$S_k = (B_{k+\frac{1}{2}}^{(n+\frac{1}{2})} + r_kQ_k)/[1 + r_kP_k + \frac{1}{4}\frac{\Delta t}{\Delta s}(v_{k+\frac{3}{2}}^{(n+\frac{1}{2})} - v_{k-\frac{1}{2}}^{(n+\frac{1}{2})}] \tag{52}$$

where

$$A_k^{(n+\frac{1}{2})} = \zeta^{(n+\frac{1}{2})} - \frac{1}{2}\frac{\Delta t}{\Delta s}[(\bar{h}^y + \zeta^x)u]_x^{n+\frac{1}{2}} \quad \text{at } j, \ k \tag{53}$$

$$B_{k+\frac{1}{2}}^{(n+\frac{1}{2})} = v^{(n+\frac{1}{2})} - \frac{1}{2} \left[\Delta t \ f + \frac{1}{2} \frac{\Delta t}{\Delta s} (v_{j+1,k+\frac{1}{2}}^{(n+\frac{1}{2})} - v_{j-1,k+\frac{1}{2}}^{(n+\frac{1}{2})}) \right] \bar{u}^{(n+\frac{1}{2})}$$

$$- \frac{1}{2} \Delta t \ gv^{(n+\frac{1}{2})} \frac{\sqrt{(\bar{u}^{(n+\frac{1}{2})})^2 + (v^{(n+\frac{1}{2})})^2}}{(\bar{h}^x + \zeta^{y(n+\frac{1}{2})})(C^y)^2} \qquad \text{at } j, \ k + \frac{1}{2} \qquad (54)$$

The recursion formulas in the y-direction are

$$\zeta_k^{(n+1)} = -P_k v_{k+\frac{1}{2}}^{(n+1)} + Q_k \tag{55}$$

$$v_{k-\frac{1}{2}}^{(n+1)} = -R_{k-1} \zeta_k^{(n+1)} + S_{k-1} \tag{56}$$

The explicit operation for the u velocity becomes

$$u^{(n+1)} =$$

$$\frac{\left\{ u^{(n+\frac{1}{2})} + \frac{1}{2} \left[\Delta t \ f - \frac{1}{2} \frac{\Delta t}{\Delta s} (u_{j+\frac{1}{2},k+1}^{(n+\frac{1}{2})} - u_{j+\frac{1}{2},k-1}^{(n+\frac{1}{2})}) \right] \bar{v}^{(n+1)} - \frac{1}{2} \frac{\Delta t}{\Delta s} g\zeta_x^{(n+\frac{1}{2})} \right\}}{\left[1 + \frac{1}{2} \Delta t \ g \frac{\sqrt{(u^{(n+\frac{1}{2})})^2 + (\bar{v}^{(n+1)})^2}}{(\bar{h}^y + \zeta^{x(n+1)})(C^x)^2} + \frac{1}{4} \frac{\Delta t}{\Delta s} (u_{j+\frac{3}{2},k}^{(n+\frac{1}{2})} - u_{j-\frac{1}{2},k}^{(n+\frac{1}{2})}) \right]}$$

$$(57)$$

The formulas developed above cannot be used directly in this form for electronic computation. Coding in FORTRAN presents problems, as coordinate description of the variables can be made only on integers, and integer-and-one-half values do appear in the formulas developed. Multiplication of all coordinate descriptions of the points by a factor of two would eliminate this problem; however, such a lattice system is uneconomical from the point of view of memory use of the computer because not all locations of an array u, v, ζ and h would be used.

It is possible to give each of the variables u, v, ζ and h a separate coordinate system, which would result in a good use of memory and would also allow coordinate description on integers. The computational formulas for these special coordinate systems and the computation program are presented in Ref. 2.

STABILITY, DISSIPATION AND DISPERSION

One of the requirements of the numerical solutions of the equations is that the obtained solutions converge to the solutions of differential equations. Also, the solutions should be stable. This can be investigated by following a Fourier expansion of a line of errors as time progresses. If this line of errors (error wave) grows with time, the computation

becomes unstable and dominates the solution. If, on the other hand, error
waves will be damped heavily if computation progresses, then, components
of the waves which we try to represent by the numerical procedures will
be damped also and possibly in a degree which is not in agreement with the
solutions of the differential equations. Such a numerical scheme is dis-
sipative. An investigation[2] of simplified sets of difference equations
(10) through (15), indicates that the multioperation method is uncondi-
tionally stable and not dissipative.

      Numerical procedures however, have influence on the phase speed of
the wave. This effect is called dispersive. The discreetness of the
representation of the waves in time and in two spatial dimensions, influ-
ences this effect. Fig. 2 shows the computed wave velocity versus the
wave velocity of the partial differential equations as function of spatial
representation for a given ratio of time and spatial gridsize. The direc-
tion of the wave compared to the grid influences this ratio. If more than
thirty points are used to represent one wavelength on the spatial grid,
then the difference between computed wave velocity and the wave velocity
of solutions of the partial differential equations are less than 1%.

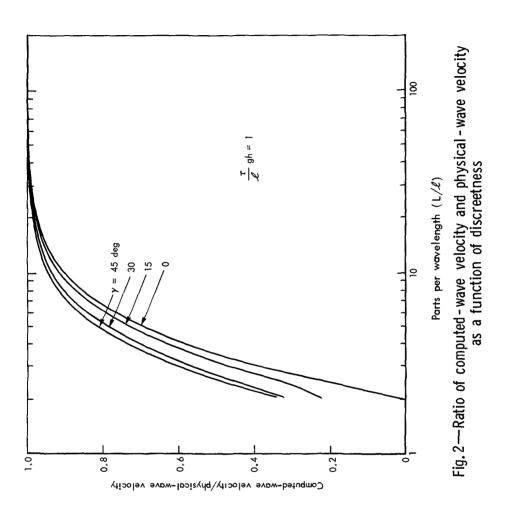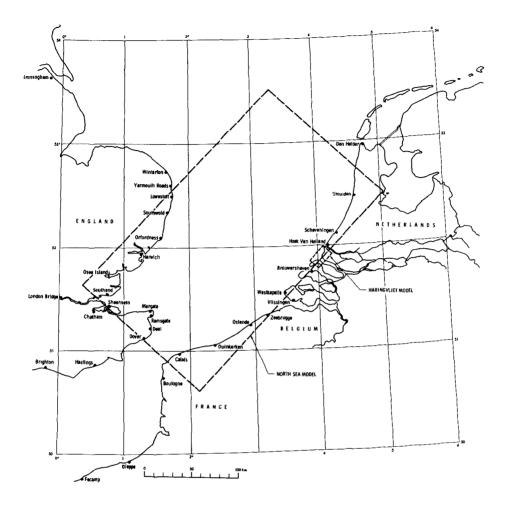   NUMERICAL EXPERIMENTS

      The model was tested by comparing measurements with computational
data. The mouth of the Haringvliet in The Netherlands was used (Fig. 3)
since detailed measurement of tidal levels and currents were available, by
The Netherlands Rijkswaterstaat, and in addition this area had large var-
iations in depth over short distances. A grid size of 400 m with a compu-
tational array of 31 by 55 points was chosen. As an aid in the evaluation
of the results, a plot program was developed for the display of currents
and water levels at certain times of the computation (Fig. 4). The values
of the Chezy coefficients were then adjusted until a good agreement was
found between measured and computed velocities and water levels (Fig. 5).
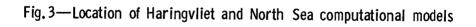A detailed description of these experiments can be found elsewhere[2].

      As a final check of the general computational procedures developed
during the experiments with the Haringvliet area, a tidal computation was
made of the southern North Sea (see Fig. 3). The gridsize used is 5600 m.

      The northern boundary of the model was described at four locations
as a time function of the water levels. Other points of this boundary
were computed by linear interpolation or extrapolation (Fig. 6). The
southern boundary in the English Channel was described at the coasts as
a time function of the water levels, and the intermediate points were com-
puted by interpolation.

      In the southwestern part of The Netherlands, currents in the differ-
ent parts of the estuaries of the Rhine and Schelde were used for the bound-
ary. Tidal data for the period from 0.00 hr (Middle European Time), September
13, 1958, were used for computation. Some adjustments were made at the be-
ginning and end of this period in order to make all tidal curves a complete
cycle over this period. The half time step of each operation was taken at
5 min. The C values were computed every half hour (real time) on the loca-
tion of the water level as a function of the average depth at that moment.

Fig. 2—Ratio of computed-wave velocity and physical-wave velocity as a function of discreetness

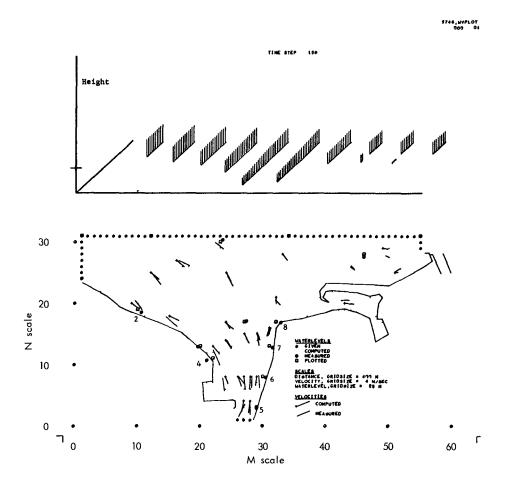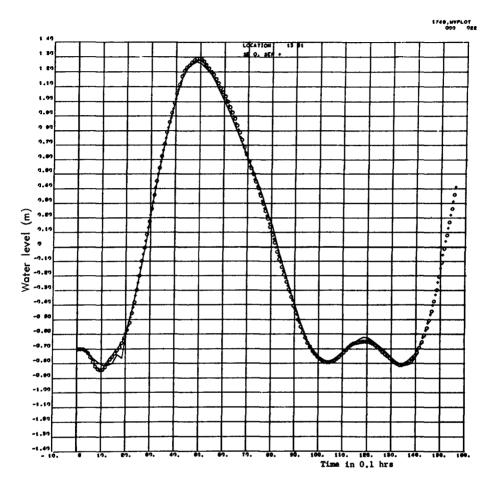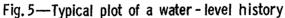Fig. 3—Location of Haringvliet and North Sea computational models

Fig. 4—Haringvliet (estuary of the Rhine)
Situation 15.6 hr (real time) after start of computation

Bottom Field of the computation and comparison between measured velocities and
computed velocities. The measured velocities are average velocities of
similar tidal cycles at a particular location, while the computed velocities
are the average velocity in an 800-by-800-m area of a particular tidal cycle.

Top Isometric sections representing computed water levels on every fifth line of
the bottom graph.

Fig. 5—Typical plot of a water - level history

Gage No. 7 Comparison between measured data (−) and computation (+0 +)
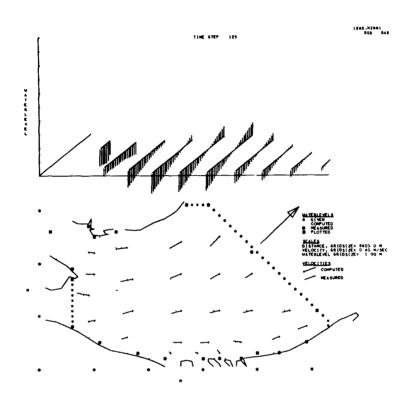
Fig. 6—North Sea computed water - levels and currents
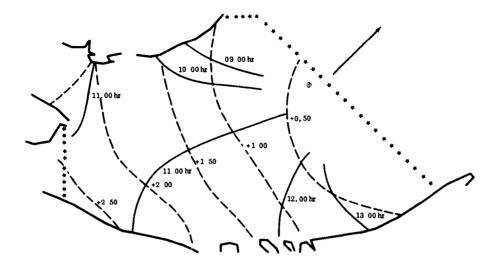on September 12, 1958 at 20.00 hr

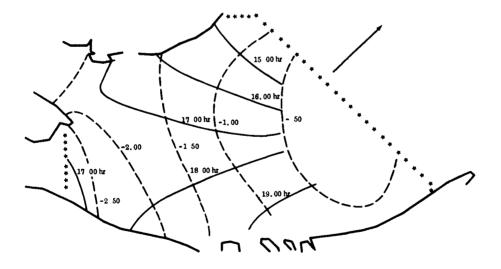Fig. 7—Iso high-tide levels and times on September 12, 1958

Fig. 8—Iso low-tide levels and times on September 12, 1958

Computations were started with all water levels and velocities taken at zero. The water levels and currents at the open boundaries were increased from zero with five steps into the given tidal curve. The starting disturbance disappeared after approximately 14 hr.

The locations of equal high-tide levels (co-range lines) obtained from the results of this computation are shown in Fig. 7, together with the arrival times of the highest water levels (co-tidsl lines). Figure 8 shows the same for the low tides. In these two figures a counterclockwise rotation of the vertical tide may be seen. The water level information shown in Figs. 7 and 8 concurs with tidal information presented by Defant[3] as to phases and smplitudes of the tides.

The maximum magnitude of the computed currents such as shown in Fig 6 agrees with information given on tidal charts, but no detailed analysis has been made of the phase and amplitude of these currents with respect to such information. Water levels and currents along the coast are not accurate as the grid size is too large for s good representation, and also more accurate input data is needed for these computations.

CONCLUDING REMARKS

It has been shown thst the propagation of long waves in coastsl waters can be studied successfully by use of a numericsl integration method. The multioperation method developed is characteristic of implicit methods; namely, there is no upper limit on the time step for stability reasons, as is the case with explicit methods. The multioperation method allows a direct and rapid solution of sll velocities and wster levels on esch time level.

The multioperation method described is particularly suitable for long-wave computation in coastal waters, where water movements are introduced by changes in the water level (or currents) along the sides of the model and where the effect of bottom friction is lsrger thsn the effects of lateral eddy viscosity, which is neglected.

The contribution of the convective-inertia terms in the equation of motion is assumed to be small compared to that of other terms. These terms are represented with a lower order of sccuracy.

The detailed description of computational procedures[2] permits an expedient introduction of geogrsphic features such as wster depth, boundaries, and characteristics of bottom roughness for the modeling of wave propagation in hydraulic engineering research.

Generally, information concerning the magnitude of the effect of bottom roughness is inadequate. In some cases, like the Haringvliet model, the water movements are influenced by bottom roughness to a considerable extent. In such a case, the parameter C has to be found in an iterative manner by comparing computed results with actual field measurements. The rate at which the model can be adjusted to resemble the prototype depends on the extent of available field data and on the experience of the engineer making the investigation and his insight into the physics of the wave problem and into the behavior of the method of numerical solution.

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