CHAPTER 96

Experimental study on on-offshore sediment transport of Accretive Beach

CHING-TON KUO* CHING-HER HWANG** I-CHOU TSENG***

1. INTRODUCTION

In treating coastal proceses, sediment transport is usually divided into along-shore and on-offshore components. It is believed that the on-offshore component has a prominant connection with short-term profile changes, observed during storm wave climates. Obviously its shift of sand plays a very vital role in shoreline migration. In other words, the beach profile has great bearing on coastal phenomena related to on-offshore sediment transport. As we know, there have been many studies on this kind of sediment transport rate, and considerable amount of knowledge on this problem has been accumulated so far. Yet it seems that we are still far from a reliable formulus to estimate the beach profile changes. The reason why is due to the complexity of mechanics of sediment transport. Therefore, the aim of this study is to examine experimentally the mechanism between onoffshore sediment transport and the deformation processes of twodimensional beach profile. Then , a predictive model of the temporal and spatial distribution of net on-offshore sediment transport based on two-dimensional beach profiles and an equation of continuity of sediment transport is proposed. Various parameters of net on-offshore sediment transport in this model are discussed also.

- * B.E., M.E., ph.D., Professor of Hydraulic and Ocean Engineering Graduate School, National Cheng Kung University, Taiwan, R.O.C.
- ** B.E., M.E., Associate Researcher, Institute of Harbor and Marine Technology, Wuchi, Taichung District, Taiwan, R.O.C.
- *** B.E., M.E., Graduate of Hydraulic and Ocean Engineering Graduate School, National Cheng Kung University, TAIWAN, R.O.C.

2. THE CONTINUITITY EQUATION OF SEDIMENT TRANSPORT

The evaluation of net sediment transport in this study was on the the basis of continuity equation of sediment transport, assume the transport mode of sediment was just bed-load and there is no suspended sediment occurred. Therefore a coaser sand of 0.57 $^{\rm mm}$ Ø was used as a bed material in order to satisfy this theoritical consideration. Usually, sediment transport rate was measured directly by a sand trap during the last few decades. But due to such apparatus would cause severe disturbance to the fluid motion and the sediment movement. Instead the net rates of sediment transport were estimated by the continuity equation from the beach deformation data comparing with the initial profile. Attemp to find temporal and spatial the relationship between the net transport rate and wave condition were then made. Suppose a beach profile changes as given in Figure 1. By virtue of the conservation of bed material amount, the local net transport rate q(x,t)per unit width is related to the bed elevation h(x,t) measured from a certain datum as :

in which $\boldsymbol{\xi}$ is the sediment porosity. Therefore the effective net transport rate $Q(\mathbf{x})$ averaged over a time duration Δt of wave action is evaluated from the bed elevation change $\Delta h(\mathbf{x})$ by

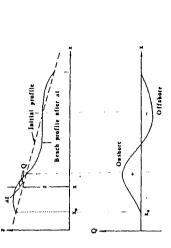
$$Q = \frac{\overline{q}}{1 - \varepsilon} = \int_{X_R}^{X' \Delta h} \Delta t \quad \dots (2)$$

where X' is positively seaward and X_R means shoreward limit of beach deformation. Parameter definition is shown as Figure 2.

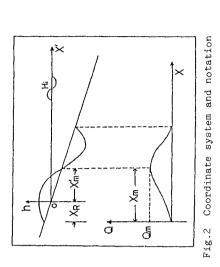
3. EXPERIMENTAL PROCEDURES

Experiments were carried out in a two-dimensional wave tank,1 m wide,1 m deep,80 m long with a glass wall on one side of 30 m length at the end of tank. Figure 3 shows the general arrangement of the test equipment.

The experiments were performed using monochromatic waves generated by a flap-type wave maker installed at another end of the tank.







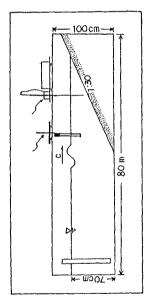


Fig.3 General arrangement of test equipment

Table-1 Experimental Conditions

	T(sec)	[H, (cm)	H./L.
AI	1.2	8.4	0.039
A2	1.2	6.7	0.031
A3	1.2	5.1	0.024
BI	1.5	12.4	0.038
B2	1.5	8.3	0.026
B3	1.5	6.1	0.019
C I	2.0	12.1	0.021
C2	2.0	8.4	0.015
C3	2.0	6.3	0.011

The incident wave height was measured by a capacitance type wave gage placed just offshore from the toe of the model beach. In order to make simply the experiments,tests were limited to a uniform initial beach profile of 1/30 and one coarse sand of 0.57^{mm} Ø was used as a bed material mentioned above. Beach profile changes were measured by an electronic profile sensor to record the continuous profile data for every two hours within the testing duration of 18 ~ 20 hrs totally. Then, the temporal and spatial net rate of on-offshore sediment transport was evaluated from the beach profile changes.

Table 1 is a list of experimental cases. Various kinds of wave conditions were investigated for this test. Both the breaker height and local wave heights were also measured by a capacitance type wave gage mounted on a carriage capable of moving with constant speed along the centerline of the tank at the locations of 50 cm interval along the model beach in the middle of wave action. The horizontal distance from a base line on the model beach to the breaking position and the limited shoreward position of run-up were measured by ruler attached on grass wall.

4. EXPERIMENTAL RESULTS & DISCUSSION

Figure 4 (a) \sim (i) show the beach profiles at the end of wave action for all the cases listed in Table 1. It should be noted that profile changes are belong to the accretive type i.e. a shoreline progresses and no sand deposition takes place offshore. (Sunamura and Horikawa, 1974). The locations of breaking points are indicated by arrow symbols; dot line arrows for the initial stage and solid line arrows for the final stage. Experimental results indicate that the locations of breaking point progress shoreward as the accumulated time of wave increased, i.e. the breaker zone become narrowed gradually as shown in Fig 5 (a) \sim (h) and its breaker type changed gradually also from spilling one to plunging breaker. Results also indicate that the maximum sediment transport rate take place arround the breaking point. Figure 6 (a) \sim (b) show some examples of the spatial and temporal distribution of the effective non-dimenssonal net transport rate Q/Qm evaluated from beach profiles mentioned above. It's seen that the

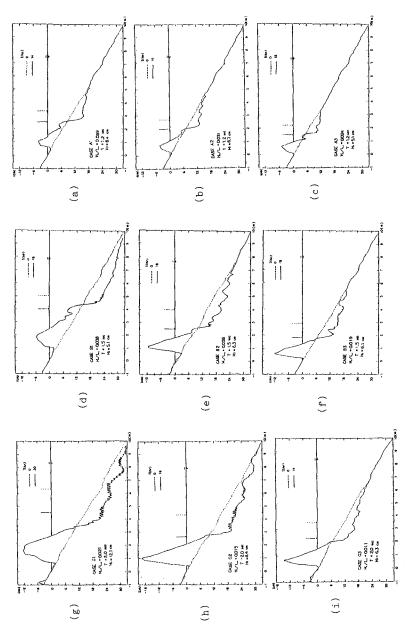
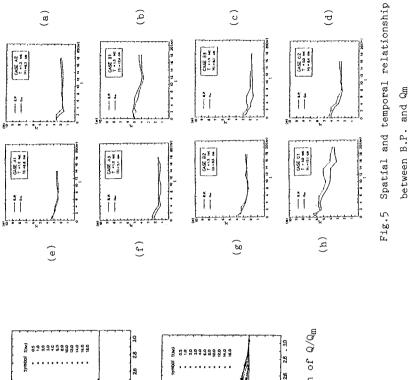
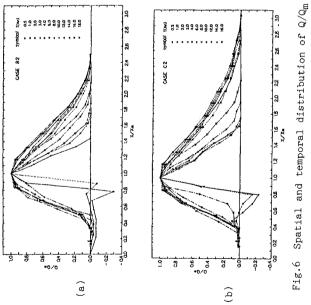


Fig.4 Beach profile after wave action





dimensionless distribution curves of sediment transport rate tend to steady after $t/T = 1.44 \times 10^4$, in which t is accumulated time of wave action and T is the incident wave period. Based on these data of each case an optimum curve was obtained to represent its characteristics as shown in Figure 7 (a)-(c). Then, a dimensionless sediment transport rate shown as Figure 8 for accretive beach were analyzed and relationship of parameters were shown also as figures 9~13. These experimental formulus were established ae follows: M-1

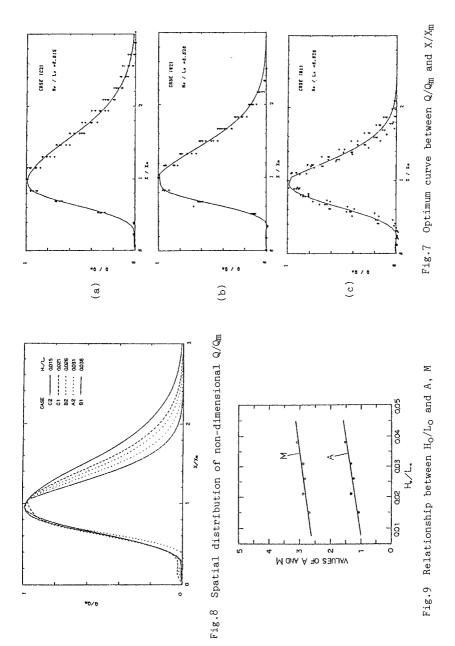
$$\begin{array}{rcl} \text{MOREL} & \text{M-1} & \text{M-1} & \text{M-1} \\ \text{Q/Qm} &= & \text{AM}\overline{X} & \text{e}^{-A\overline{X}} & \text{; } \overline{X} > 1 & \dots & \dots & (3) \\ \text{Q/Qm} &= & \text{C}_{6} \overline{X}^{6} + & \text{C}_{5} \overline{X}^{5} + & \text{C}_{4} \overline{X}^{4} + & \text{C}_{3} \overline{X}^{3} + & \text{C}_{2} \overline{X}^{2} + & \text{C}_{1} \overline{X} + & \text{C}_{0} & \text{; } \overline{X} < 1 \\ \text{and} & & \\ \text{C}_{6} &= & 32.31 & \text{, } & \text{C}_{5} &= & -87.96 & \text{, } & \text{C}_{4} &= & 79.23 & \text{, } & \text{C}_{3} &= & -25.38 \\ \text{C}_{2} &= & 2.81 & \text{, } & \text{C}_{1} &= & 0.01 & \text{, } & \text{C}_{6} &= & 0.00 \end{array}$$

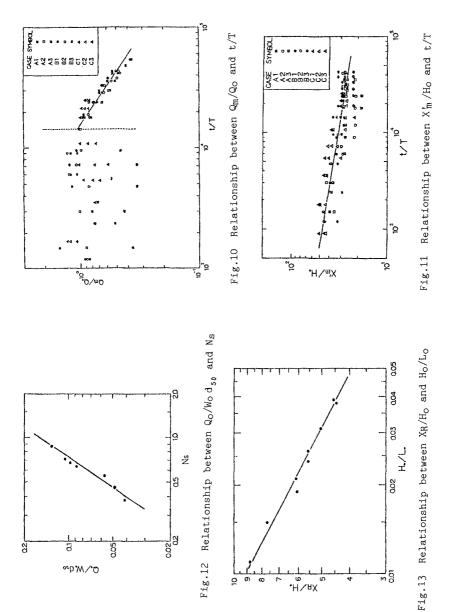
 $A = 15.16 ({^{Ho}/_{Lo}}) + 0.89$ $M = 13.55 ({^{Ho}/_{Lo}}) + 2.52$ (4)

in which

$$\begin{split} \overline{\mathbf{X}} &= \mathbf{X}/\mathbf{X}_{m} \\ \mathbf{Q}_{m}/\mathbf{Q}_{o} &= 478.6 \ (^{t}/_{T}) \ ^{-0.64} \ ; \ ^{t}/_{T} \ \geq 1.44 \ \times \ ^{10^{4}} \dots (5) \\ \\ \mathbf{Q}_{o}/_{Wod \mathbf{so}} &= 0.16 \ \mathrm{Ns}^{1.51} \dots (6) \\ \\ \mathrm{Ns} &= \ ^{H}/_{T} \ / \ \sqrt{(\mathrm{s-1})\mathrm{gd}_{\mathbf{so}}} \dots (7) \\ \\ \mathrm{Xm}'/_{\mathrm{Ho}} &= 141.3 \ (^{t}/_{T})^{-0.16} \ ; \ ^{t}/_{T} \ \geq 1.44 \ \times \ ^{10^{4}} \dots (8) \\ \\ \mathbf{X}_{R}/_{\mathrm{Ho}} &= 0.771 \ (^{\mathrm{Ho}}/_{\mathrm{Lo}})^{-0.537} \dots (9) \end{split}$$

Where





1320

Ns = dimensionless parameter

5. APPLICATION OF THE NUMERICAL MODEL

Based on These experimental formulus mentioned above, then, a numerical model of two-dimensional accretive beach profile changes is presented. Figure 14 (a) \sim (c) are the examples of the comparison between this predictive numerical model and experimental results; solid line represents the numerical computational values and dot line represents the experimental results after 20 hours of wave action. Results indicate that the numerical model could be used to describe adequately on-offshore beach profile changes for the accretive beach.

6. CONCLUSIONS

The main conclusions of this study are summarized as follows: (1) Experimental results indicate that final beach profile changes after 14 \sim 20 hrs wave action respectively for all the cases are belong to the accretive type, i.e. a shoreline will progresses seaward and no sand deposition takes place offshore and predominant mode of sediment transport is the bed-load. (2) When the time of wave action was increased, the breaker zone width will become narrower and narrower and its breaker type will change gradually also from spilling one to plunging breaker. (3) Results indicate that the position of maximum sediment transport rate will take place around the breaking point. (4) On-offshore sediment transport rate is the function of Ns and t/T, and could be expressed as equation (3) to equation (9). When the acaumulated time of wave action are greater than t/T =1.44 $\times 10^4$, its normalized non-dimensional spatial distribution of sediment transport rate could tend to be steady. (5) Based on the experimental results, a predictive numerical model is presented and shown that this model could be used to describe adequately the on-offshore beach profile changes for acroetive beach.

7. ACKNOWLEDGEMENTS

The authers wish to expressed their gratitude to all of them who carried out this study. And thanks to the national scientific

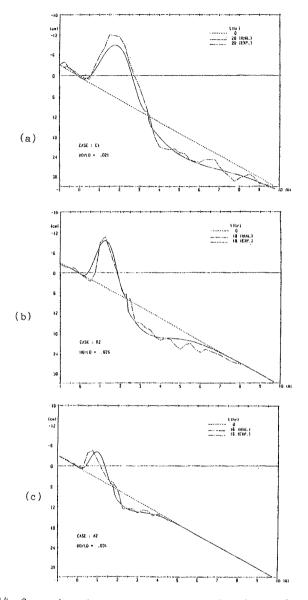


Fig.14 Comparison between numerical model and experimental results

council to support funds under the contact NSC 74-0410-E006-02. Authers would also like to thank Miss Joanna Chang IHMT to type.

8.REFERENCES

pp. 1439-1458.

SAWARAKI T. & DEGUCHI I. (1980). On-offshore sediment transport rate in the surf zone., Proc of the 17th Conference on Coastal Engineering, Chapter 73, pp. 1194-1214. WATANABE, RIHO & HORIKAWA(1980). Beach profiles and on-offshore sediment transport., Proc of the 17th Conference on Coastal Engineering, Chapter 68, pp. 1106-1121. HATTORI M. & KAWAMATA R. (1980). On-offshore transport and aeach profile changes., Proc. of the 17th Conference on Coastal Engineering, Chapter 72, pp. 175-1192. HATTORI M. (1982). Field study on On-offshore sediment transport., Proc. of the 18th Conference on Coastal Engineering pp. 923-939. BAILARD J.A. (1982). Modelling On-offshore sediment transport in the surf zone. Proc. of 18th Conference on Coastal Engineering, PP. 1419-1438. SHIBAYAMA T. & HORIKAWA K. (1982). Sediment Transport and beach transformation., Proc of 18th Conference on Coastal Engineering,