BEACH NOURISHMENT AS A MANAGEMENT TECHNIQUE

David M. Chapman,
Coastal Studies Unit,
University of Sydney, Australia

## 1) INTRODUCTION

Beach nourishment is considered an environmentally safe manage-
ment technique, since an unsuccessful nourishment project would
simply result in the redistribution of borrow material by wave action
into environments more in keeping with a state of equilibrium. No
permanent modifications of the beach and nearshore environment need
result, and since no permanent structures are required for beach
nourishment, the management commitment allows rapid project abortion
if necessary. Beach nourishment monitoring has usually been concerned
with evaluating changes in the extent of subaerial beach and/or re-
tention of fill volume. These parameters are important, but it is
also necessary to consider the way in which nourishment sand is taken
up by the beach system since relationships between volume change,
change in extent of subaerial beach, and changes in beach morphology
are complex. This paper is concerned with evaluating beach nourish-
ment on the Gold Coast (Figure 1), Australia's major resort, where
2.4 million cubic metres of fill were applied in the largest beach
nourishment project attempted in this country at the time of writing.

Methodology, reported in Chapman & Smith (1977) and Chapman
(1978a) included repetitive profile survey from backshore to point of
zero change in inshore zone (over 400 profiles) using highly accurate
techniques, and use of 38 tonnes of tracer, which was injected into
the dredge line at a controlled rate.

## 2) BEACH BEHAVIOUR

### 2.1 Width/Volume Relationships

Analysis of Gold Coast survey data showed that subaerial (or
"dry") beach width, taken alone, is a poor indicator of the volume of
sand present in the active zone, or swept prism (Chapman & Smith,
1980), and is therefore not a reliable index of resistance to erosion.
Correlation of subaerial beach width, per se, and sand prism volume
is poor, and comparisons only become meaningful if beach morphologic
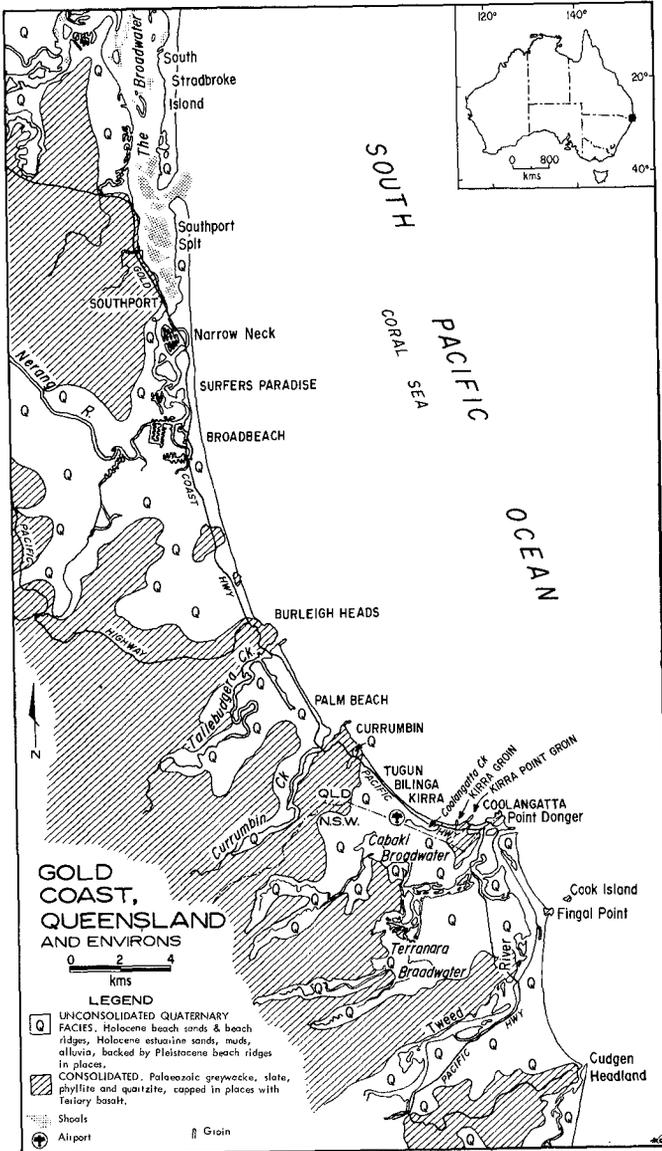states are taken into consideration.

FIGURE 1

Net change in volume of the Lower Gold Coast beaches following
nourishment is shown in Figure 2, with change in width of the sub-
aerial beach shown in Figure 3.  Datum in both cases is the beach
state at commencement of survey.  Although a net gain of volume
occurred, Fig. 2 demonstrates that distribution of change at end of
survey was very uneven, with the bulk of the fill remaining close to
the delivery point in the form of two large "slugs", or parcels of
sand.  Comparison of Figures 2 and 3 also shows the importance of the
subaqueous profile (or in-shore zone).  Shoreline changes do not re-
flect the true state of erosion or accretion following beach nourish-
ment.  The total sand volume contained in the nourished area is
critically dependent on the subaqueous profile.  Shoreline recessions
may be accompanied by accretion of the subaqueous profile.  The lack
of correlation between Figs. 2 & 3 is significant, showing as it does
that width of subaerial beach is not a good indication of sand storage
in the total beach system.

The large slug of sand centred on 2500 metres is almost wholly
contained in the subaqueous part of the profile, being poorly reflected
in added beach width, whilst small gains in beach width at 2000 metres
and 3,500 metres do not reflect added volume in the beach prism at
these points, but rather the reverse is true.

Most of the active zone of the beach is subaqueous (Chapman &
Smith, 1980);  a wide subaerial beach may give a deceptive appearance
of security to resource managers, since the widest subaerial beach
for a given fixed volume of sediment in the active zone, is associated
with fully accreted, highly reflective beach states (cf. Short, 1978;
Wright, et al., 1979).  Beaches in this condition are very sensitive
to sudden increase in wave power, which causes rapid transfer of sed-
iment to the subaqueous beach, and corresponding loss of subaerial
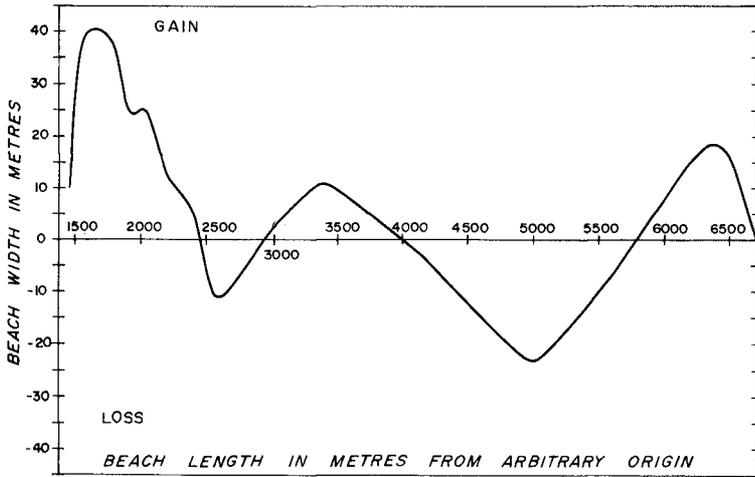beach width.

Re-distribution of beach sand by high energy waves was observed
on the Lower Gold Coast seven months after project completion, when
tropical cyclone "David" crossed the shoreline at about Lat $24^{\circ}S$.
A reduction in dry beach width of over 20m occurred over the study
area, with overall gradient being reduced from approx. 1:40 to approx.
1:80.  The volume of the swept prism (Chapman & Smith, 1980) remained
unchanged.

2.2  Manner of Sand Movement

It was found that the phenomenon of slugs of sand discussed
above was not restricted to the nourishment project.  Slugs of sand
have been observed at three scales:  (a)  small-scale irregularities
in beach volume revealed by survey as in Fig. 2;  (b)  medium-scale
parcels of several hundred thousand cubic metres, usually associated
with the flushing of flood-tidal deltas from estuarine inlets, and
their subsequent accession to adjacent beaches;  and (c) large-scale
slugs of a million cubic metres or more, which appear as somewhat
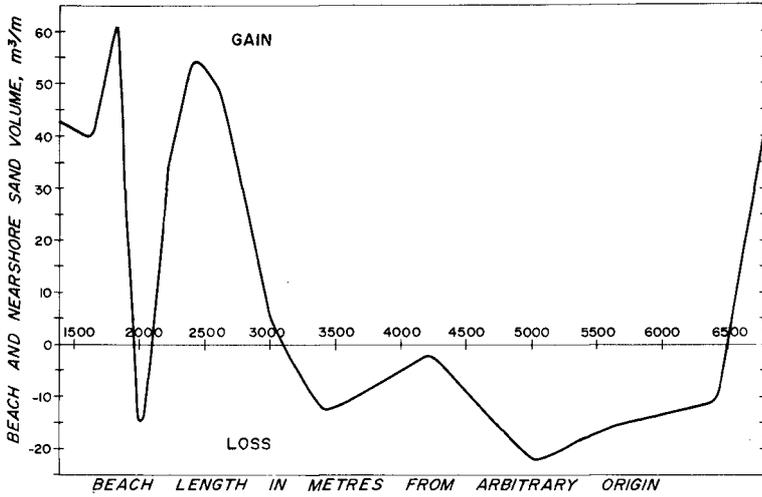
CHANGE IN BEACH AND NEARSHORE SAND VOLUME

FIGURE 2



CHANGE IN BEACH WIDTHS, KIRRA - CURRUMBIN

FIGURE 3

subtle, low amplitude variations in subaerial and subaqueous sand storage over beach lengths of several kilometres.

Longshore transport, both in the short term of the nourishment monitoring study, and the longer term of some years, was effected by the alongshore migration of these slugs rather than as a continuous longshore flow of sand. Small and medium scale slugs tended to retain their identity whilst moving alongshore (drift direction is south-to-north, or left to right in Figs. 2 &3) for distances of one or two kilometres, but then to diminish in amplitude and to coalesce into large-scale slugs.

Observations of large-scale slug movement, made over a period of 10 years, have revealed the slow longshore progression of forms illustrated schematically in Figure 4. Drift direction is from left to right; longshore movement of identifiable forms is indicated by the oblique arrows. The alongshore movement of the slugs of fill material from Kirra ($1.0 \times 10^6 m^3$) and Surfers' Paradise ($1.4 \times 10^6 m^3$) was particularly evident, since, although diffused with native sand, the fill slugs still exhibited a slightly different hue compared with the native sand in 1980. Calculations of volumes present in the slugs and rates of movement of their centroids indicated that longshore transport volume effected thereby was of the order of $2.0 - 2.5 \times 10^5 m^3 yr^{-1}$, a result remarkably similar to the figures of 2.84 and $2.52 \times 10^5 m^3 yr^{-1}$ derived for the Lower Gold Coast by intensive volumetric survey and tracer analysis (Chapman, 1978b).

The phenomenon of shore-parallel sediment movement in the form of discrete slugs has also been reported from the New Jersey coast of the U.S., where slugs of wavelength 4000-5000m were observed by Everts (pers. comm.)

2.3  Nourishment and Beach Topography

Fill application to the Lower Gold Coast resulted in a beach and inshore morphologic response similar to that observed on the beach sections adjacent to estuarine inlets following flushing by floods of flood-tidal deltas of marine sand contained in them, viz., amorphous inshore shoals, expansion of surf zone width, highly dissipative (as defined by Wright, et al., 1979) conditions, and considerable wave setup.

As the slugs of fill moved alongshore, intensified and persistent rips developed ahead of them, leading to loss of beach width and volume as revealed in Figures 2 & 3. It is thought that a longshore gradient of radiation stress associated with wave setup over the fill slugs may have contributed to scour at the downdrift toe. The intensified rip at 3600 metres from the origin locally modified wave behaviour in the course of a short and relatively minor storm such that wave attack caused sea-wall collapse and property erosion behind the cell.
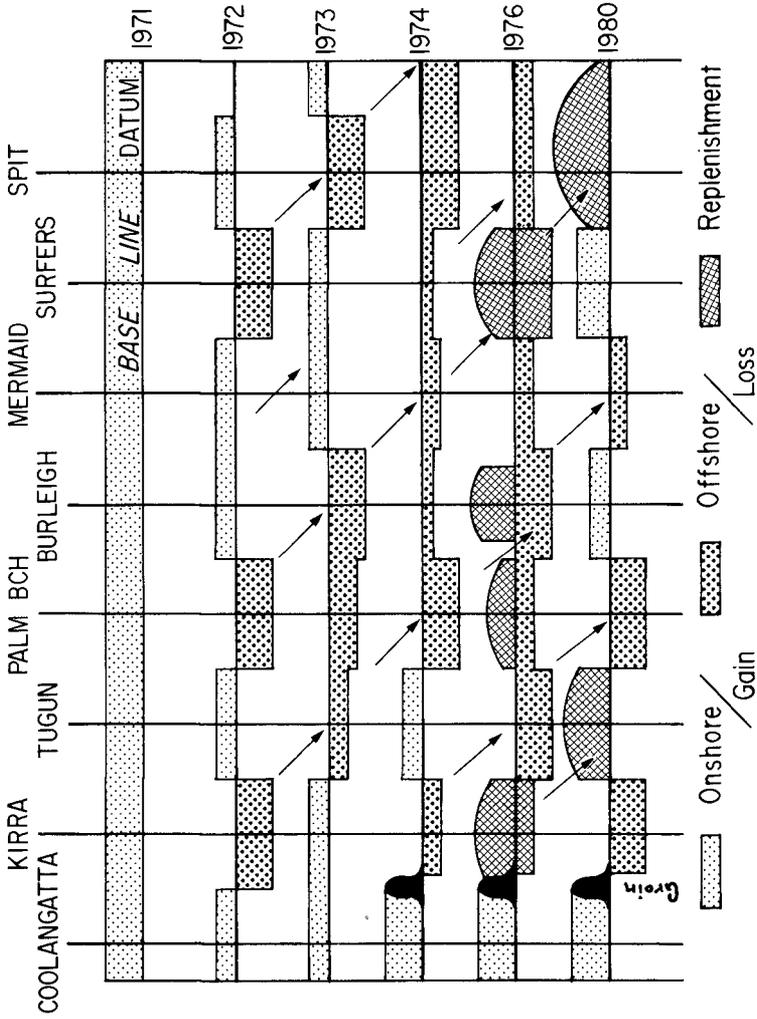
FIGURE 4

The phenomenon of scour at the downdrift end of fill on the Lower Gold Coast did not occur at the site of the contemporaneous nourishment project at nearby Surfer's Paradise. At Surfer's Paradise, it was more convenient for the contractor to place the fill by extending the delivery pipe incrementally in the <u>opposite</u> direction to the longshore transport system. No perturbations at the downdrift end of the nourished beach were observed.

## 3)  FILL SELECTION & PLACEMENT

### 3.1  <u>Fill Evaluation Criteria</u>

<u>A priori,</u> one might expect that nourishment sand should be texturally matched to native sand if the "artificial" beach is to be successful. It may be anticipated that erosive forces would be less competent to remove sand of a coarser texture, hence use of nourishment sand substantially coarser than native might be expected to produce a more durable beach. Newman (1976) for example, considered that nourishment sand should have a median diameter $1\frac{1}{2}$ – 2 times that of native sand, and the well-known <u>critical ratio</u> concept has been developed around the foregoing assumption (Krumbein and James, 1965) to define the ratio of volume of nourishment sand required to be placed to the volume retained on the beach in equilibrium with shore processes. In most cases critical ratios considerably exceed unity, predicting that the proposed borrow material is less than ideal and that winnowing will selectively remove unsuitable fractions of the fill until it becomes compatible with the existing beach regime.

An alternative approach to evaluating the modification of nourishment sand by beach processes was proposed by James (1975), in the form of the <u>re-nourishment factor</u> which attempts to predict frequency of re-nourishment and to evaluate the long-term performance of proposed fill materials with regard to suitability, maintenance, and expense. The active beach system is considered a compartment which gains sediment through longshore transport and from gradual erosion of the store of sediments forming the backshore, and loses sediment by longshore and offshore transport beyond its boundaries. Fill is viewed as an increase to the backshore store. Sediment particle residence time in the compartment is longer for coarse grained material than for fine; thus a comparison between composite size distributions of native and borrow sediments is used to predict the "lifetime" of fill. A renourishment factor of $\frac{1}{2}$ means that borrow material would be expected to erode at half the rate of native material; renourishment with such borrow material should be required half as often as renourishment with sediment of identical composition to native material. Conversely a renourishment factor of 2 indicates that renourishment would be required twice as often as would be the case if native type sediment were used. The renourishment factor increases with an increasing difference between native and borrow means; the finer the borrow material compared with native, the higher the predicted retreat rate. Poorly sorted borrow material results lower predicted retreat rate since it contains a larger fraction of coarser material which is considered to provide a stable armour.

As the textural correspondence between native and borrow materials used in the Lower Gold Coast project was almost perfect , both the critical ratio and renourishment factor formulae gave values close to unity. However, using data derived from sediments actually present within the dynamic swept prism (Chapman & Smith, 1980) of the Lower Gold Coast, sensitivity analyses made on the formulae cast doubt on their validity. Aggregated samples varied between the limits (mean = 2.0$\phi$, s=0.4$\phi$) and (mean = 2.5$\phi$, s=0.5$\phi$), a remarkably homogeneous sand body; nevertheless both the critical ratio and renourishment formulae predicted that one or the other of these materials would generate quite marked changes in beach behaviour* in an environment where both were demonstrably in equilibrium.

Losses of beach nourishment material have often been ascribed to supposed winnowing of the finer fraction of such material, with the assumption that the fine sediment is lost to the system. Such is not neccessarily the case, for, if a beach is moved into a different state by fill application, and redistribution of material to the inshore and inner nearshore takes place as a result, introduced material is not lost, but merely distributed in a different way to native material. In many cases the "lost" material will still be found within the dynamic swept prism (Chapman & Smith, 1980); absolute loss presupposes the existence of a sink. Accession of fill to the subaqueous part of the swept prism may produce a beach of lower overall gradient, with but slight increase in width, but one in which the swept prism has the capacity to absorb a great deal of wave energy without substantial withdrawal of sand from the subaerial part of the prism.

Introduction of finer-than-native material may well shift the beach regime into a more dissipative regime (cf. Wright, et al, 1979) with wider inshore zone, which could, by causing greater frictional dissipation of wave energy at greater distance from the backshore than in the pre-fill state, enhance erosion resistance. The fine sand, highly dissipative beach also requires more wave energy, compared to other beach states, to produce substantial erosion (Wright, 1980).

Use of coarser-than-native material, on the other hand, could conceivably cause a shift to a more reflective beach regime associated with a narrower inshore zone; this beach state is the one most delicately poised and subject to rapid collapse and removal of sand from the subaerial beach with input of increased wave energy (Wright, et al., 1979).

However, Gold Coast experience indicates that diffusion of fill into native sand may be rapid enough to warrant consideration of a new sand population formed as a mixture of fill and native materials. For the first two months after commencement of fill delivery, advection of added volume occurred principally over the first 1.5 km downdrift of the input point (Fig. 2) but diffusion of nourishment sand was very rapid, and revealed a high degree of over-turning within the sand prism.

---

* e.g. the renourishment factor varied between 0.41 and 1.92 in tests cited

Coring of the prism and analyses of tracer concentration (Chapman & Smith 1977) that the ratio of nourishment to native sand could be described by $r = e^{-(y-0.1)}$ where $y$ is distance alongshore in kilometres.

Fill evaluation formulae as discussed above also presuppose the loss of the finest sand from the beach system. However, many microscopic examinations of beach sediments from a wide range of energy environments in eastern Australia have invariably revealed a significant tail of very fine sand, even in the extreme case where phi mean approached zero. Since Hobson & James (1978) have shown that elutriation of fines not in equilibrium with the beach environment can be very rapid, the persistent presence of very fine tails in beach sands suggests that these form part of the normal populations of the beaches concerned. Work in progress also suggests that behaviour of the sediments may be related to the frequency distribution of specific surface, as distinct from mean diameter (Smith & Gordon, 1980), in which case the fine tail achieves greater prominence.

The critical ratio and renourishment factor concepts appear to have evolved from the perception of a wide subaerial beach as the most desirable state, and assume uniform profile retreat under erosion. Rather than searching for field data for verification of the concepts, as has been suggested (e.g. Dean, 1976) it may be that criteria are required for the evaluation of fill suitability in terms of its effect on beach morphology within a given energy environment.

3.2 Fill Placement

Fill placement has usually been thought of in terms of a design profile of beach nourishment distribution (Delft, 1970; Silvester, 1974; Vallianos, 1975). Silvester suggested the calculation of an "equilibrium" profile form, whilst Vallianos used the concept of a design profile, complete with shaped dune form. Experience from the Gold Coast suggests that, whilst the design profile concept may be useful for calculation of fill quantities, it is of little value as a practical working criterion for the reconstruction of beaches by means of nourishment, since the procedure assumes both fill retention and morphology are predictable.

The concept of an artificially shaped profile, complete with formed dune, was an essential element in the scheme for the Gold Coast (B.P.A., 1973). The sand supplied to the beach was to be distributed above high water level by bulldozer and vegetation was to be established upon an artificially formed dune. The design concept envisaged that the fill would be placed as high on the beach as possible, covering any boulder walls present, and allowing the surplus only to escape to the swash zone.

However, execution of the concept proved impractical. Emplacement of fill sand in the design profile meant that the unnaturally high "berm" was scarped at high tide. This not only gave the public the impression that fill was being lost by erosion, but made beach access

difficult for swimmers which resulted in public relations problems for
the Local Authority.

　　　The artificially formed "dune" concept also proved impractical.
Immediately upon drying out, sand began to drift onto the backshore
and enroach upon parking areas and esplanades. Moreover, attempts at
establishment of the sand-binding grass, Spinifex hirsutus, in the
pumped sand proved abortive. The tight packing characteristics and fines
content of pumped sand were dissimilar to the lightly packed, free mov-
ing sand of the normal accreting foredune. It appears that the dissim-
ilarity was great enough to inhibit Spinifex development.*

　　　Much of the literature on beach management is imbued with static
notions of beach equilibrium. The beach must be recognised as a dynamic
system, and managed within its dynamic range, for management to be
effective. The concept of the equilibrium inshore profile was shown
by Chapman (1978b) to be a chimera. Use of an appropriate three-dimens-
ional model allows a number of more-or-less discrete beach stages (or
equilibria) to be recognized, as described by (e.g.) Short (1978) or
Wright, et al., (1979). Viewed in this context, management of a beach
by means of nourishment involves more than merely the addition to the
active zone of sand having a suitable 'critical ratio' or 'renourishment
factor'. Manipulation of the beach system could involve consideration
of the characteristic morphologic states of the beach in question with
their probabilities of occurrence spatially and temporally and in
relation to most probable energy inputs. Given a variety of possible
sediment sources it may be possible to induce beach behaviour of more
dissipative or more reflective modes if these were considered desirable.
Timing of application of nourishment with respect to existing or prob-
able morphologic states and energy inputs, both from sea and wind, in
order to maximise fill utility and encourage formation of backshore
dunes, also may be seen as a management variable.

4)　CONCLUSION

　　　To the lay beach user, or even to the resource manager unfamiliar
with inshore morphodynamics, a wide subaerial beach is interpreted as
a sign of the presence of a large sediment volume. Results reported
above show this perception may be quite erroneous.

　　　A commonly applied guideline of one square foot of beach area
gained per cubic yard of fill, may be seen in its general form as an
attempt to relate subaerial beach area to volume of the sand prism;
however it was shown above that width (or area) of subaerial beach is

---

* S.hirsutus is propagated by seed. Vegetative propagation is possible
but not practical. The popular Ammophila spp. used in many cool temp-
erate areas, A. Arenaria and A. breviligulata, were unsuitable for the
Gold Coast as the sub-tropical location is beyond the environmental
tolerance of the latter species.

poorly correlated with volume in the sand prism. Width will depend,
inter alia, on beach state and on texture of added sediment.

Commonly-used renourishment factor or critical ratio concepts are
unsoundly based;  since both use simplistic data as basic input they
can at best provide over-simplified approximations of the complex and
dynamic beach regime, and no process terms are included in either.
Basic to both concepts is the assumption that a coarser-than-native
sediment is desirable for fill purposes, and is likely to prove more
stable under the wave climate of the problem area. Whilst coarser
non-cohesive sediment is less likely to be moved by any given wave than
is fine sediment, it does not necessarily follow that coarser sediment
will ultimately produce a more stable beach or more desirable beach
state than native material.

A beach will be built, by waves, of whatever suitable material
is available;  high energy wave climates are not necessarily always
associated with beaches of coarse sediment, or vice versa.

Sediment size is but one of a matrix of factors responsible for
beach behaviour at a site under any given wave climate;  varying sand
grainsize may simply cause a shift into a different stage in the mor-
phodynamic continuum rather than producing a beach of different erosion
resistance.

The design profile concept is useful for computing required fill
amounts by comparison with existing beach profiles;  however, it assumes
that both fill retention and morphology are predictable and that the
design profile can be constructed. In practice, in a moderate-to-high
energy environment, the concept may be operationally impractical, and
establishment of vegetation by seed in pumped-sand "dunes" proved
difficult. Fill redistribution by natural marine and aeolian processes
proved more effective and economic than attempts to create an idealised
profile. Apparent "losses" from the dry beach were accounted for by
redistribution in the inshore zone.

Perturbations of the inshore system caused by fill application
may affect local erosion patterns and longshore transport in ways
which would be unexpected from observation of the beach in its normal
state. Radiation stress gradients developed as a result of topography
associated with nourishment may lead to intensified erosion adjacent
to the filled beach.

If fill redistribution within the dynamic swept prism is seen as
normal, and the movement of sediment to the subaqueous part of the
prism as morphodynamic change rather than loss of material, it may be
possible to consider a wide variety of potential nourishment sources
to increase the erosion resistance of a given beach, and even to think
of "tuning" to achieve desirable morphologic states.

5) REFERENCES

B.P.A. (1973) Scheme Prepared by the Beach Protection Authority pursuant to the Beach Protection Act 1968-1970 for the Protection of all Beaches Situated at the Gold Coast. Brisbane, The Authority, 8pp. + maps.

CHAPMAN, D.M. (1978a) Management of Sand Budget, Kirra Beach, Gold Coast. 4th Aust. Conf. Coastal & Ocean Eng., pp. 19-24. The Institution of Engineers, Australia.

CHAPMAN, D.M. (1978b) Management of Sediment Budget. Lower Gold Coast. Queensland. Ph.D. Thesis, University of Sydney, 279pp.

CHAPMAN, D.M., SMITH, A.W. (1977) Methodology of a large scale tracer experiment. 3rd Aust. Conf. Coastal & Ocean Eng., pp. 185-189. The institution of Engineers, Australia.

CHAPMAN, D.M., SMITH, A.W. (1980) The dynamic swept prism. Proc. 17th Coastal Eng. Conf., ASCE.

DEAN, R.G. (1976) Beach erosion - causes, processes, and remedial measures. CRC Crit. Reviews in Envir. Control, 6 (3) 259-296.

DELFT HYDRAULICS LABORATORY (1970) Gold Coast, Queensland, Australia-Coastal Erosion and Related Problems; Report 257 in 2 vols, Delft, The Laboratory.

HOBSON, R.D. JAMES, W.R. (1978) Importance of handling losses to beach fill design. Proc. 16th. Coastal Eng Conf., ASCE, pp. 1873-1887.

JAMES, W.R. (1975) Techniques in evaluating suitability of borrow material for beach nourishment. TM60, U.S. Army Coastal Engineering Research Center, Fort Belvoir, VA.

KRUMBEIN, W.C. JAMES, W.R. (1965) A lognormal size distribution model for estimating stability of beach fill material. TM 16, U.S. Army Coastal Engineering Research Center, Washington, DC.

NEWMAN, D.E. (1976) Beach replenishment - sea defences and a review of the role of artificial beach replenishment. Proc. Inst.n Civ. Engrs., 60: 445-460.

SHORT, A.D. (1978) Wave power and beach stages - a global model. Proc. 16th. Coastal Eng. Conf., ASCE, pp. 1145-1162

SILVESTER, R. (1974) Coastal Engineering. 2 vols., Amsterdam, Elsevier

SMITH, A.W., GORDON, A.D. (1980) Secondary Sand Transport Mechanisms Proc. 17th Coastal Eng. Conf., ASCE

VALLIANOS, L. (1975)  Beach–fill planning, Brunswick County, North Carolina. pp 93–114 in Hayden, B.P. (ed) <u>The Present   and Future of Coasts</u>. Proc. 1st. Ann. Conf. Coastal Soc., Bethesda, M.D., The Society.

WRIGHT; L.D. (1980)  Modes of beach cut in relation to surf–zone morphodynamics.  <u>Proc. 17th Coastal Eng. Conf.</u> ASCE

WRIGHT, L.D., CHAPPELL, J., THOM, B.G., BRADSHAW, M., COWELL,P. (1979) Morphodynamics of reflective and dissipative beach and inshore systems, southeastern Australia.  <u>Mar. Geol.</u> 32:105–140.